Stratigraphic in version of poststack PS converted waves data

A lejandp A. Valenciano and Reinaldo J. Michelena^{*}, PDVSA-Intevep

Summary

We show in this paper that conventional, poststack stratigraphic inversion of PS converted waves based on the convolutional model for the seismic trace yields impedance estimates, pseudo S-w aveimpedances, that are the product of a pseudo density by S-wave velocity. This pseudo density transforms the equation for the PSreflection coefficient for near vertical incidence into an expression that is equivalent to the well-known expression of the normal incidence reflection coefficient for P-waves. The pseudo density is a function of the medium density and the V_P/V_S ratio. The dependence of the angle in the PS reflection coefficient is eliminated when stacking and, therefore, near offset stacked PS traces can be modeled and inverted assuming the convolutional model for the seismic trace. We also derive a simple expression to estimate medium density that depends on $V_P V_S$, V_P/V_S , P-wave impedance, and pseudo S-wave impedance estimated all from conventional velocity analysis and stratigraphic inversion of near offset PP and PS data.

Introduction

The estimation of medium properties from changes in P-wave reflectivity has been performed successfully during many years using not only poststack data when w e want to estimate changes in P-wave impedance (Russell and Hampson, 1991), but also prestack data when w ew antto estimate changes in S-w avevelocities and densities that affect the reflectivity at large offsets (Demirbag et al., 1993).

The estimation of changes in medium properties from PS converted waves, how ever, is commonly performed using only prestack data (Stewart, 1991). The reason for not using poststack PS converted waves to estimate danges in medium properties because we have not been able to find a model for PS stacked data that has the simplicity of the convolutional model we assume tomodel PP stacked data. Unlike PP reflectivity, PS reflectivity is zero for normal incidence and, therefore, the convolution of the normal incidence reflectivity series with a wavelet is meaningless as a way to model PS stacked data.

We show in this paper that near offset PS stacked data can be approximated by the convolution of the near normal incidence PS reflectivity $[R_{PS}(\theta \approx 0)]$ with a wavelet. Even though the PS reflectivity is zero for normal incidence, we demonstrate that the stacked trace we assign to the common conversion point location is proportional to changes in a quantity that we defined as a pseudo S-wave impedance. This quantity is obtained after replacing the density term in the appro ximation of the PS reflection coefficient $R_{PS}(\theta \approx 0)$ by a new pseudo density. This new density transforms $R_{PS}(\theta \approx 0)$ into an expression that has the same functional form as the *P*-w ave normal incidence reflection coefficient. We also derive an expression for the density of the medium that depends on the product and ratio of interval V_P and V_S velocities and the product of the pseudo *S*-w ave impedance and the *P*-w ave impedance. A simple synthetic example demonstrates the validity of the new approximations.

Near offset PS forward modeling

According to Aki and Ric hards (1980), the expression for the *PS*-wavereflection coefficient on a solid-solid interface betw een medium 1 and medium 2 is

$$R_{PS} = -\frac{V_P}{2V_S} \tan \psi [A \frac{\Delta \rho}{\rho} - B \frac{\Delta V_S}{V_S}], \qquad (1)$$

where

$$A = 1 - 2\frac{V_S^2}{V_P^2}\sin^2\theta + 2\frac{V_S}{V_P}\cos\theta\cos\psi,$$

and

$$B = 4 \frac{V_S^2}{V_P^2} \sin^2 \theta - \frac{4V_S}{V_P} \cos \theta \cos \psi.$$

The angle θ is the incidence angle of the *P*-w are and ψ is the emergence angle the *PS* converted wave. This equation is valid when ΔV_P , ΔV_S , and $\Delta \rho$ are all small.

F or small angle of incidence θ , we can approximate equation 1 of the PS-w ave reflection coefficient as

$$R_{PS} \approx -2\sin\psi \left[\left(\frac{1}{4} \frac{V_P}{V_S} + \frac{1}{2} \right) \frac{\Delta\rho}{\rho} + \frac{\Delta V_S}{V_S} \right].$$
(2)

As we can see, for positive contrasts of medium properties across the interface, the PS-wave reflection coefficient is negative for near vertical rays, unlike the reflection coefficient for normally inciden tP-waves which is always positive for positive contrasts of medium properties

Similarly to near offset P-w avetraces, near offset PSw avetraces can be approximated as the convolution of PS-wave reflectivity series

$$r_{PS}(t) = \sum_{i}^{N} R_{PSi}(\psi_i) \delta(t - \tau_{PSi})$$

with a wavelet W_{PS} as follows:

$$t_{PS}(t) \approx r_{PS}(t) * W_{PS}(t), \qquad (3)$$

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where N is the total number of interfaces and τ_{Psi} indicates the position in time of the i^{th} interface.

The *PS*-wave stacked trace T_{PS} is obtained after integrating equation 3 from zero to the converted wave angle ψ_m that corresponds to the farthest trace in the NMO corrected, common conversion point gather. The result is

$$T_{PS}(t) \approx 2(\cos\psi_m - 1) \sum_{i}^{N} \left[\left(\frac{1}{4} \frac{V_{Pi}}{V_{Si}} + \frac{1}{2} \right) \frac{\Delta\rho_i}{\rho_i} + \frac{\Delta V_{Si}}{V_{Si}} \right] \delta(t - \tau_{PSi}) * W_{PS}(t), \qquad (4)$$

which means that, after assigning all scale factors to a new wavelet \widehat{W}_{PS} , the stacked trace of the horizontal component of the geophone can be approximated by

$$T_{PS}(t) \approx \sum_{i}^{N} \left[\left(\frac{1}{4} \frac{V_{Pi}}{V_{Si}} + \frac{1}{2} \right) \frac{\Delta \rho_{i}}{\rho_{i}} + \frac{\Delta V_{Si}}{V_{Si}} \right] \widehat{W}_{PS}(t - \tau_{PSi}).$$
(5)

As we can see, the stack of the horizontal component of the geophone (equation 5) produces an average trace that contains information about changes in medium properties, whic his also the case for the stack of near offset vertical component traces. How ever, the main difference betw een these t w o cases is that foP-w aves the stak is also proportional to the reflection coefficient at zero offset whereas for PS-w aves it is not, since the PS-wave reflection coefficient is zero for normal incidence. As Stewart et al. (1998) point out, stac led PS sections represent an average of the amplitude versus offset response across the set of offsets that enter into the common conversion point gather.

There areman y commercial software packages available today to estimate P-waveimpedance from PP data. Ho wever, if we want to use the same tools with PS data, we need to transform the equation of the PS reflection coefficient in such a way it has the same functional form as the PP reflection coefficient. Next section explains this change in detail.

Estimation of pseudo S-waveimpedance

The equations for the near vertically inciden tPP- and PS-waves respectively have similar dependence on both velocity and density changes. These equations, how ever, are not functionally identical because the factor that multiplies the changes in density differs from one equation to the other. If we want them to be equivalent, we need to find a quantity $\hat{\rho}$ proportional to density such that

$$\frac{\Delta\rho}{\widehat{\rho}} = \left(\frac{1}{4}\frac{V_P}{V_S} + \frac{1}{2}\right)\frac{\Delta\rho}{\rho}.$$
(6)

After assuming small changes in density across the interface, the integration of equation 6 yields the pseudo densit $\mathbf{y}\hat{\rho}$ we were looking for (which has no units of density):

$$\widehat{\rho} = \rho^{\left(\frac{1}{4}\frac{V_P}{V_S} + \frac{1}{2}\right)}.$$
(7)

After replacing ρ from equation 7 into equation 2 (remembering that $\Delta \rho / \rho \approx \Delta \log \rho$), we obtain

$$R_{PS} \approx -2\sin\psi \left[\frac{\Delta\widehat{\rho}}{\widehat{\rho}} + \frac{\Delta V_S}{V_S}\right],\tag{8}$$

which is an expression equivalent to the normal incidence reflection coefficient for P-w aves except for the term $\sin \psi$ that factors out after stacking. As shown in Sheriff and Geldart (1982), this expression can be also expressed as

$$R_{PS} \approx -2\sin\psi \frac{\widehat{Z}_{S2} - \widehat{Z}_{S1}}{\widehat{Z}_{S2} + \widehat{Z}_{S1}},\tag{9}$$

where $\widehat{Z}_{Sj} = \widehat{\rho_j} V_{Sj}$ is the pseudo S-wave impedance. Therefore, if we perform conventional stratigraphic inversion (Russell and Hampson, 1991) of PS stacked data, we obtain estimates of \widehat{Z}_S . Only for the cases when the density does not dange vertically or when $V_P/V_S = 2$, the pseudo S-w ave impedance coincides with the actual S-w ave impedance.

Estimation of density

After estimating P-w ave impedance and pseudoS-w ave impedance from stratigraphic inversion of PP and PSdata respectively, we can easily show that the medium densit y can be estimated from near offset data by using the expression

$$\rho = \left(\frac{Z_P \widehat{Z}_S}{V_P V_S}\right)^{\frac{1}{\alpha}},\tag{10}$$

where

$$\alpha = \frac{1}{4} \frac{V_P}{V_S} + \frac{3}{2}.$$
 (11)

The density estimate we obtain from equation 10 is consistent with both PP and PS data. However, it requires independent estimates of V_PV_S and V_P/V_S that can be obtained either from a dipole sonic log or from interval velocities obtained after conventional v elocit analysis of PP and PS data. The ratio V_P/V_S can be estimated also from interval traveltimes by using the well known formula

$$\frac{V_P}{V_S} = 2\frac{\Delta t_{PS}}{\Delta t_P} - 1, \tag{12}$$

where Δt_{PS} and Δt_P are the traveltime differences betw een top and bottom of the interval of interest. Equation 10 is obtained after multiplying $Z_P = \rho V_P$ by $\hat{Z}_S = \hat{\rho} V_S$. Other expressions for ρ can be obtained by combining Z_P and \hat{Z}_S in different ways.

Synthetic example

T o test the ideas presented in previous sections, we generated synthetic PP and PS reflectivities using the

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exact expressions of the Zoeppritz equations (Aki and Ric hards, 1980). To model the synthetic data, we used real dipole sonic log velocities and densities from a w ell located in eastern Venezuela.

Figures 1 and 2 show the PP and PS reflectivities calculated for angles betw een 1 and 30 degrees. The purpose of this modeling was to simulate the range of angles that enter into a typical stac ked trace for PP and PS seismic records. After stac king the reflectivities for all angles, we used the recursive formula (Russell and Hampson, 1991)

$$Z_{j+1} = Z_j \frac{1+R_j}{1-R_j} \tag{13}$$

to estimate the corresponding impedances Z_P and Z_S . In order to use equation 13, we needed to be careful about selecting the proper scaling of the reflection coefficients. Figures 3 and 4 show the results of the recursive inversions, which are *P*-wave and pseudo *S*-wave impedances. We observe that real and estimated impedances (solid and dashed curves respectively) are in close agreement with each other, which confirms that stratigraphic inversion of *PS* records yields the pseudo *S*-wave impedances introduced in equation 9.

Finally, we used the estimated *P*-wave and pseudo*S*-wave impedances to estimate the density of the medium. Figure 5 sho ws that the densitiesestimated using equation 10 reproduce very w ell the real ones. After some experimentation, we found that this formula is not too sensitive to variations in V_P/V_S , and good density estimates can be obtained using only average V_P/V_S values.

Conclusions

We have demonstrated that poststack PS converted w avescan be inverted for pseudo impedances that are the product of S-wave w avevelocities and a pseudo density that equals the medium density for the case $V_P/V_S = 2$. For other values of V_P/V_S , this pseudo density transforms the equation of the PS reflection coefficient for small angle of incidence into an equation that is functionally identical, except for an angle factor, to the well known expression of the PP normal incidence reflection coefficient.

Impedances derived from poststack inversion of PP and PS data can be combined inv arious ways into a single expression to estimate the density of the medium. The particular expression for the density proposed in this paper depends, besides impedances, on the product and the ratio of P- and S-w av velocities.

We have tested the validity of the new approximations with synthetic data generated using real velocities, real densities, and the exact expressions of the Zoeppritz equations. However, more research needs to be done to understand the advantages and difficulties of using this formulation to invert real, poststac k converted aves data.

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Fig. 1: Synthetic P-w ave reflectivity R_{PP} for angles betw een 1 and 30 degrees.

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1 and 30 degrees.

Fig. 2: Synthetic PS-w ave reflectivity R_{PS} for angles bet ween Fig. 4: Comparison betw een real and estimated pseudoS-w ave impedances.

800



- real 900 1000 1100 depth (feet) 1200 1300 1400 1500 1600^L 1.9 2.2 2.1 2.3 2.4 2.5 2 density (g/cm3)

impedances.

Fig. 3: Comparison between real and estimated P-wave Fig. 5: Comparison between real and estimated densities using equation 10.